

System Examples

Filters, Cables, and Transmission Lines

Updated:2/25/15

Outline

Remember: Linear Time Invariant System

- An electronic filter or system is **linear** when superposition holds

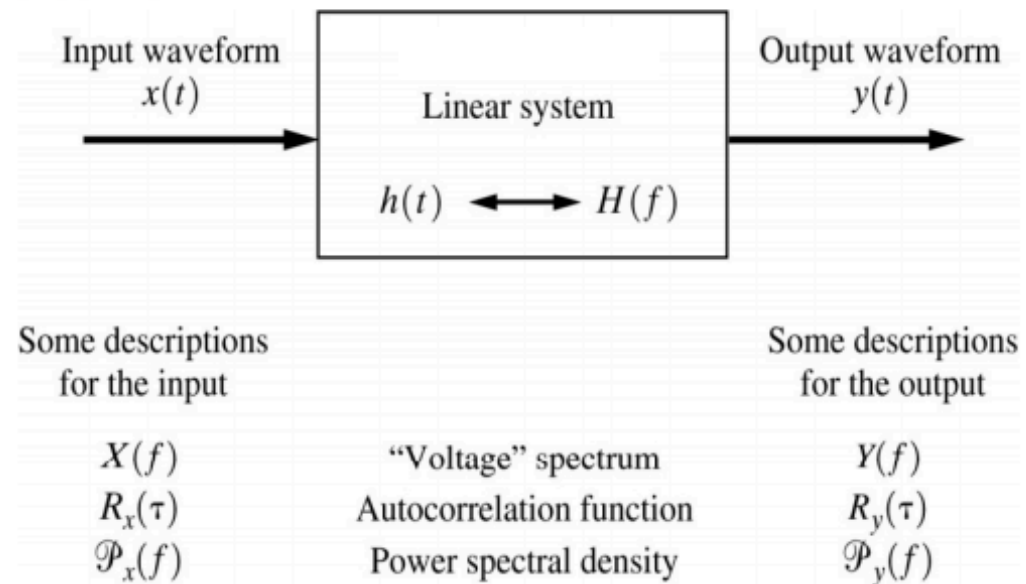
$$y(t) = L[a_1x_1(t) + a_2x_2(t)] = a_1L[x_1(t)] + a_2L[x_2(t)] \quad L \text{ is a Linear Operation}$$

where $a_1x_1(t) + a_2x_2(t)$ is the input & y is output.

- Note that the above satisfies both scaling & superposition properties.
- The system is **time invariant** if, for any delayed input $x(t - t_0)$, the output is delayed by the same amount $y(t - t_0)$.

– Shape of response stays the same.

Example:
 $y(t) = t - 3$
 Is a linear time invariant system



Linear Time Invariant System (LTIS)

- **Transfer Function:** The spectrum of output is obtained by taking FT of both sides of $y(t) = x(t) * h(t)$, i.e.,

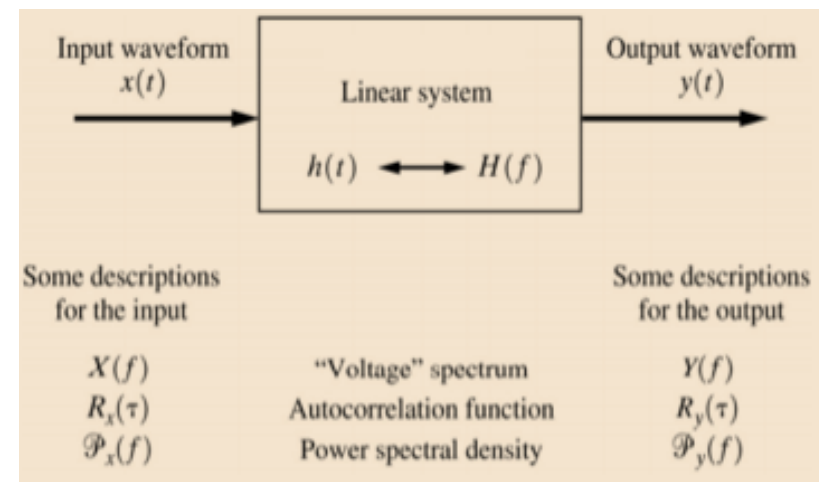
$$Y(f) = X(f)H(f), \text{ or } H(f) = \frac{Y(f)}{X(f)}$$

$H(f) = F[h(t)] =$ Transfer Function *or* system frequency response

$$H(f) = |H(f)| e^{j\angle H(f)}, \angle H(f) = \tan^{-1} \left[\frac{\text{Im} [H(f)]}{\text{Re} [H(f)]} \right]$$

- Since $h(t)$ is real,

$|H(f)|$ is an even function &
 $\angle H(f)$ is an odd function of frequency.



Example: RC Low-Pass Filter Characterization

- In the RC LP filter,
 $x(t) = Ri(t) + y(t)$, where

$$i(t) = C \frac{dy}{dt}, \text{ or } x(t) = RC \frac{dy}{dt} + y(t)$$

- Taking FT of both sides

$$X(f) = RC(j2\pi f)Y(f) + Y(f), \text{ or}$$

$$H(f) = \frac{Y(f)}{X(f)} = \frac{1}{1 + j2\pi fRC}, \text{ and}$$

$$h(t) = \begin{cases} \frac{1}{\tau_0} e^{-t/\tau_0}, & t \geq 0, \tau_0 = RC \\ 0, & t < 0 \end{cases}$$

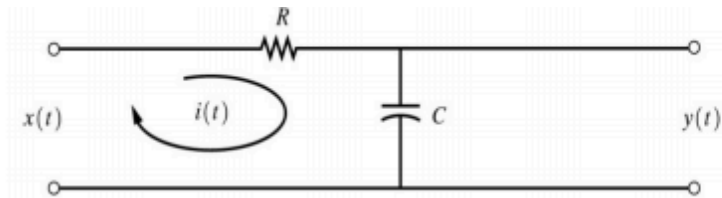
See Fourier Pair Table (Exponential one-sided)

$RC = \text{Time Constant}$, $f_0 = 1/(2\pi RC)$.

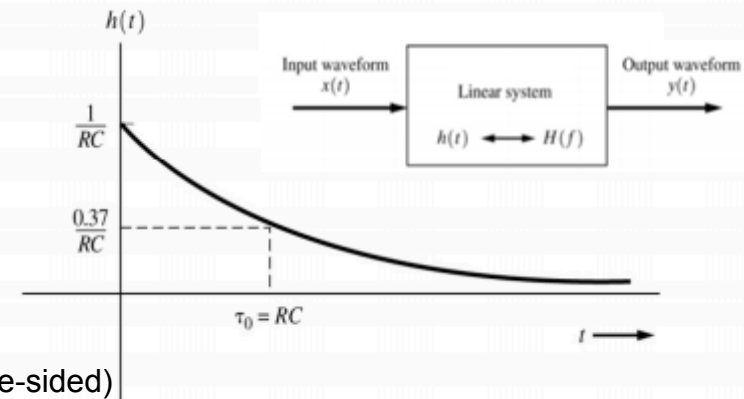
Power Transfer Function

$$G_h(f) = |H(f)|^2 = \frac{1}{1 + (f/f_0)^2}$$

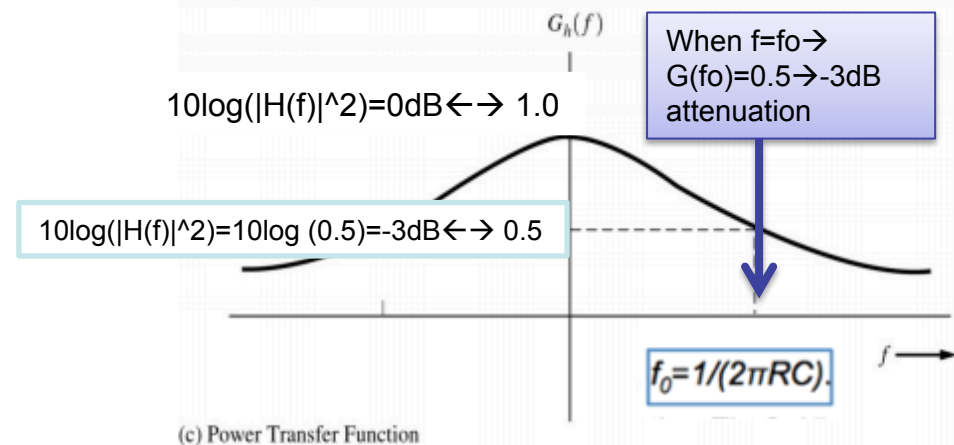
- Power gain at $f = f_0$ is $G_h(f_0) = 1/2$.
- Output is attenuated by 3-dB $f = f_0$.



(a) RC Low-Pass Filter



(b) Impulse Response



(c) Power Transfer Function

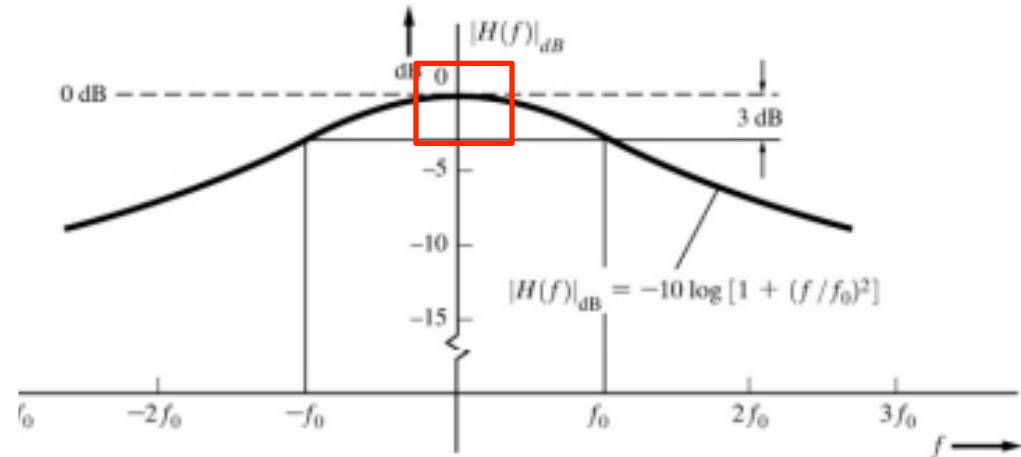
Is the Output of an RC Filter Distortionless?

Remember, for RC filter:

Power Transfer Function

$$G_h(f) = |H(f)|^2 = \frac{1}{1 + (f/f_0)^2}$$

- Power gain at $f = f_0$ is $G_h(f_0) = 1/2$.
- Output is attenuated by 3-dB $f = f_0$.



- What is the distortion effect caused by an RC low-pass filter?

- The amplitude & phase are

$$|H(f)| = \frac{1}{\sqrt{1 + (f/f_0)^2}}, H(f)_{dB} = -10 \log_{10}[1 + (f/f_0)^2]$$

$$\theta(f) = \angle H(f) = -\tan^{-1}(f/f_0)$$

- The time delay function is

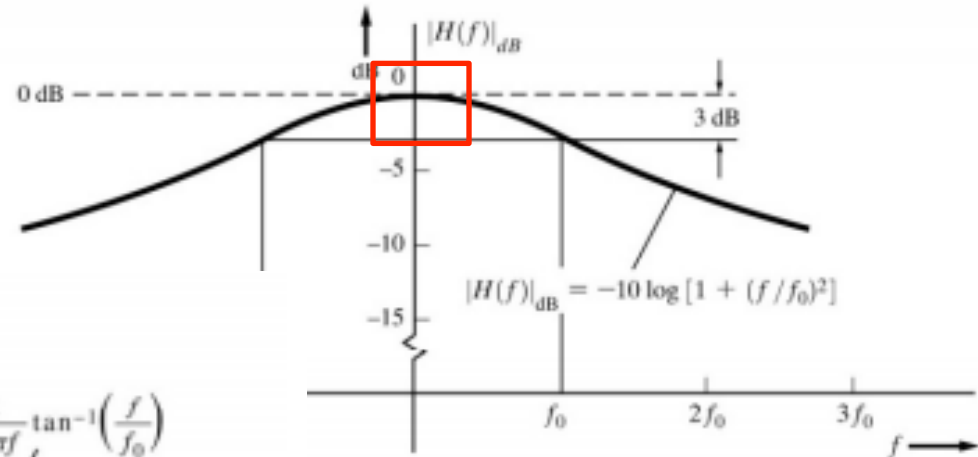
$$T_d(f) = \frac{1}{2\pi f} \tan^{-1}(f/f_0)$$

Introducing both amplitude and phase distortion!

...see next

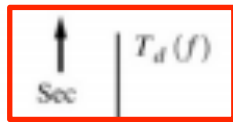
Is the Output of an RC Filter Distortionless?

Amplitude distortion if the amplitude response is not flat

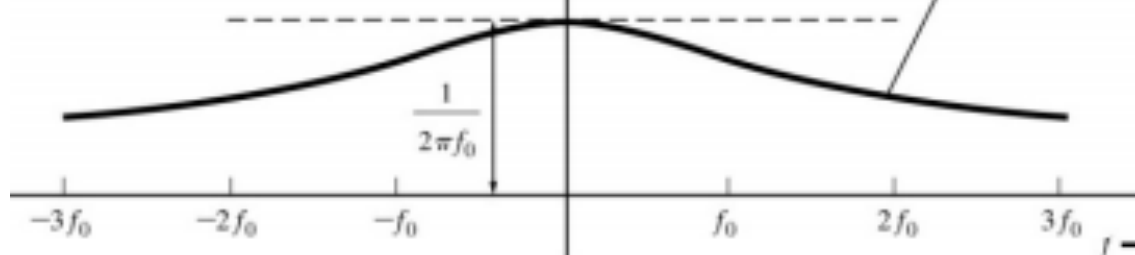


- The time delay function is

$$T_d(f) = \frac{1}{2\pi f} \tan^{-1}(f/f_0)$$

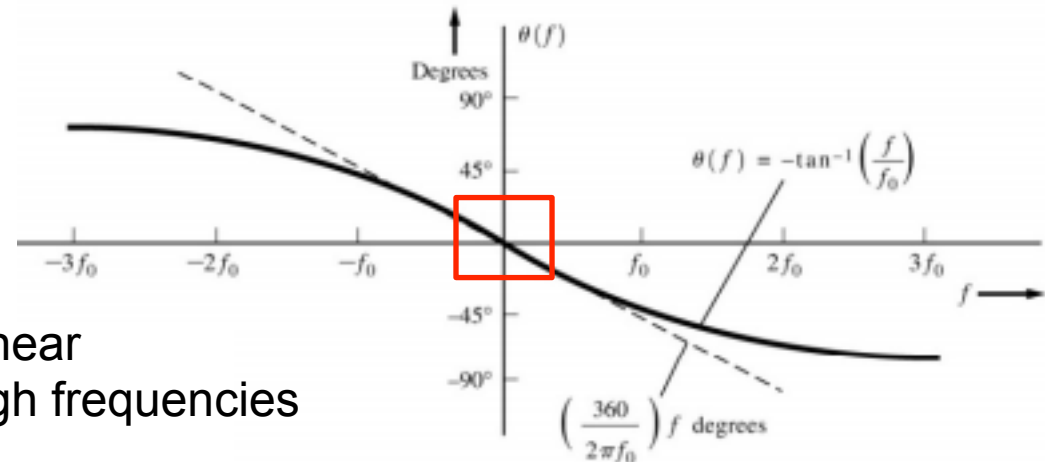


$$T_d(f) = \frac{1}{2\pi f} \tan^{-1}\left(\frac{f}{f_0}\right)$$



Range of frequencies ($<0.5f_0$) where (almost) no distortion occurs:
For example: If $f_0=10\text{KHz}$, @
 $T_d(1\text{KHz})=1/2\pi f_0=0.2$ msec delay;
producing small percentage of phase error.

Phase response is not a linear function of frequency at high frequencies

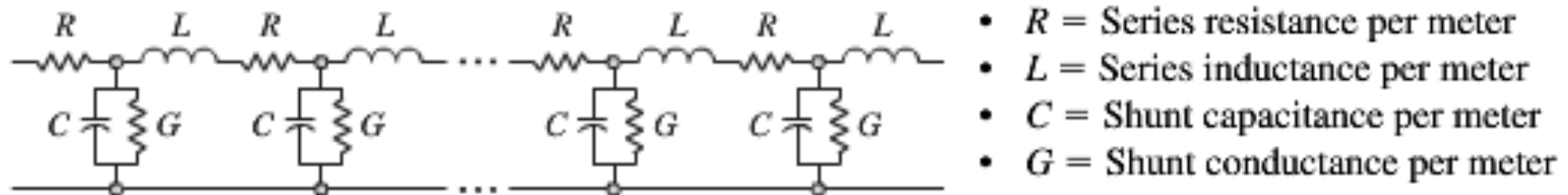


Distortion Transmission

- An LTI system is termed **distortionless** if it introduces the same attenuation to all spectral components and offers linear phase response over the frequency band of interest
- Types of distortions
 - Amplitude
 - Group delay
 - Phase delay

Cable Characterization

- Find frequency domain characterization of twisted wire pairs (TWP) and coaxial cables → use transmission line theory concepts
- Transmission line theory concepts:



- The transmission line is lossless if $R = G = 0$
- At high frequencies $R(f) \approx c_o \sqrt{2\pi f}$
 - This is due to skin effect: tendency of high frequencies in a signal to travel near the surface of a conductor in a layer some tens of microns thick

Propagation Constant

- If voltage $x_i(t)$ is applied at the input to the transmission line at time $t=0$, the voltage along the line declines exponentially with distance over time t :

$$x(z, t) = Ae^{j2\pi ft}e^{-\gamma z} \quad \text{at time } t$$

- The propagation constant is a complex function of frequency and is given in terms the lumped-circuit model element values as

$$\gamma(f) = \alpha(f) + j\beta(f) = \sqrt{(R + j2\pi fL)(G + j2\pi fC)}$$

- where α = attenuation coefficient (it is 0 for lossless line), and β =phase shift coefficient $=2\pi/\lambda$ (radians/meter).

Characteristic Impedance

- Another important parameter of the transmission line is its characteristic impedance, Z_0
- Z_0 is defined as the input impedance of an infinite line or that of a finite line terminated with a load impedance, $Z_L = Z_0$.
- Z_0 is given in terms the lumped-circuit model element values as

$$Z_0 = \sqrt{\frac{R + j2\pi fL}{G + j2\pi fC}}$$

- Thus, the transfer function $H_{TWP}(f, \ell)$ is given by

ℓ is in km!!

$$H_{TWP}(f, \ell) = e^{-\gamma(f)\ell}$$

α is the real part of prop. const

- The **attenuation or insertion loss** is defined as the reduction or loss in signal power as it is transferred across the transmission medium & it is determined by the magnitude of its transfer function,

$$|H_{TWP}(f, \ell)| = e^{-\alpha(f)\ell}$$

TWP Attenuation

- For high frequencies:
- Thus, for
- For TWP
- It turns out that

$$f \geq 300 \text{ kHz}, \alpha(f) \approx c_1 \sqrt{f}$$

$$|H_{TWP}(f, \ell)| = e^{-\alpha(f)\ell}$$

$$\alpha(f) = c_1 \sqrt{f} + c_2 f$$

$$f \geq 300 \text{ kHz}, \alpha(f) \approx c_1 \sqrt{f}$$

- c_1 and c_2 Parameters
For popular TWP Cables

Type	c_1	c_2
Cat 3	4.31×10^{-3}	4.26×10^{-7}
Cat 4	3.89×10^{-3}	4.82×10^{-7}
Cat 5	3.83×10^{-3}	2.41×10^{-8}
AWG 26	4.8×10^{-3}	-1.71×10^{-8}
AWG 24	3.8×10^{-3}	-0.54×10^{-8}
AWG 22	3.0×10^{-3}	0.035×10^{-8}

- Thus, the attenuation of TWP is usually expressed in dB as

$$\text{Insertion Loss} = -20 \log_{10} |H_{TWP}(f, \ell)| = -20 \log_{10} e^{-\alpha(f)\ell} = 8.686 \alpha(f) \ell \text{ dB}$$

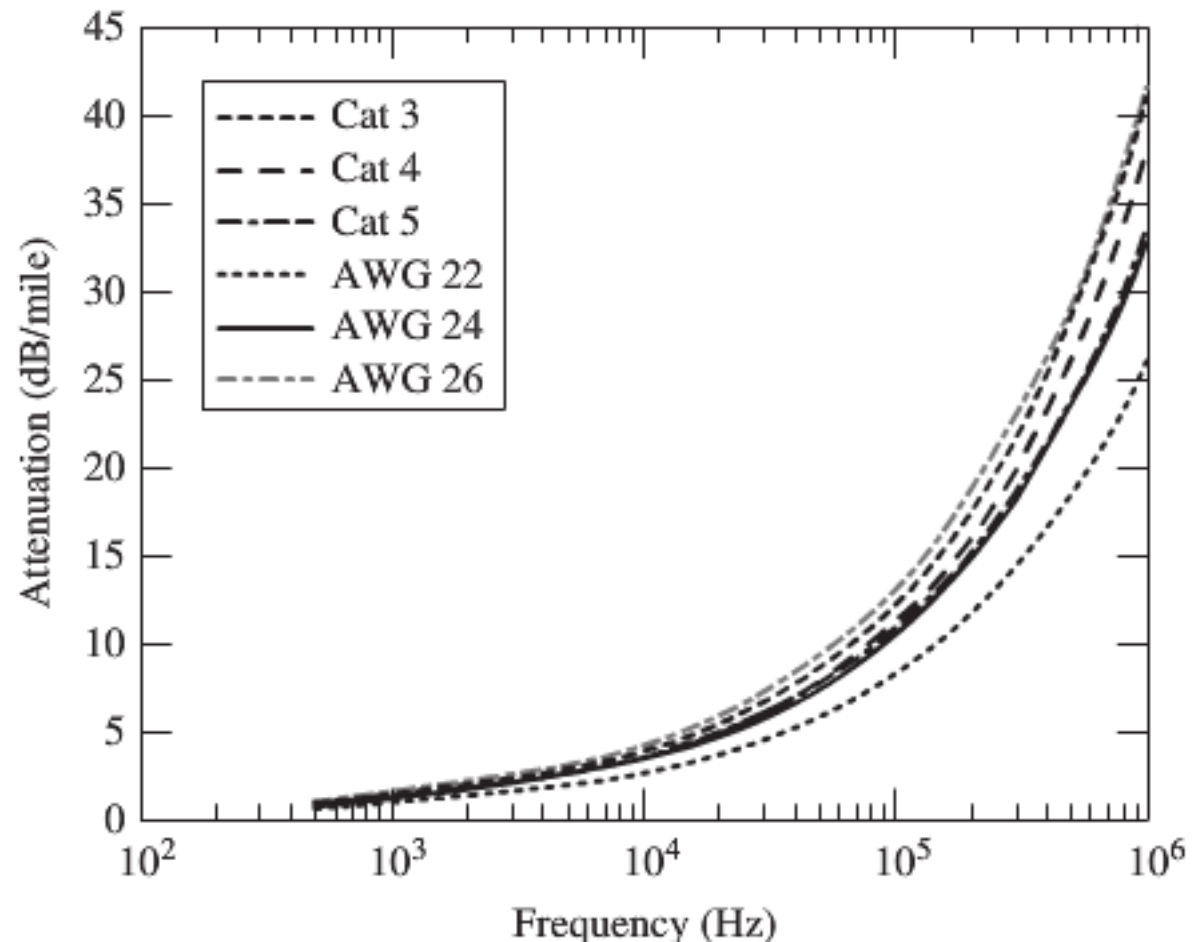
- Note: where f and ℓ , are specified in Hz and miles, respectively.

TWP Attenuation

- Remember:

$$\text{Insertion Loss} = -20 \log_{10} |H_{TWP}(f, \ell)| = -20 \log_{10} e^{-\alpha(f)\ell} = 8.686 \alpha(f) \ell \text{ dB}$$

- Note that larger ℓ
 - Results in more Loss
 - limiting the BW!



Example 1:

- Consider a 2-pair 24-AWG TWP
- We often use this cable to connect the subscribers & limited to 18,000 feet drops (about 5.45 km).
- Determine the output of 6-km TWP for an input sinusoidal signal $5 \cos(6800\pi t)$, that is $f=3200$ Voice signal



$$C = 0.05 \mu\text{F}/\text{km}$$

$$L = 0.673 \text{ mH}/\text{km}$$

$$R = 180 \text{ ohms}/\text{km}$$

$$G = 0$$

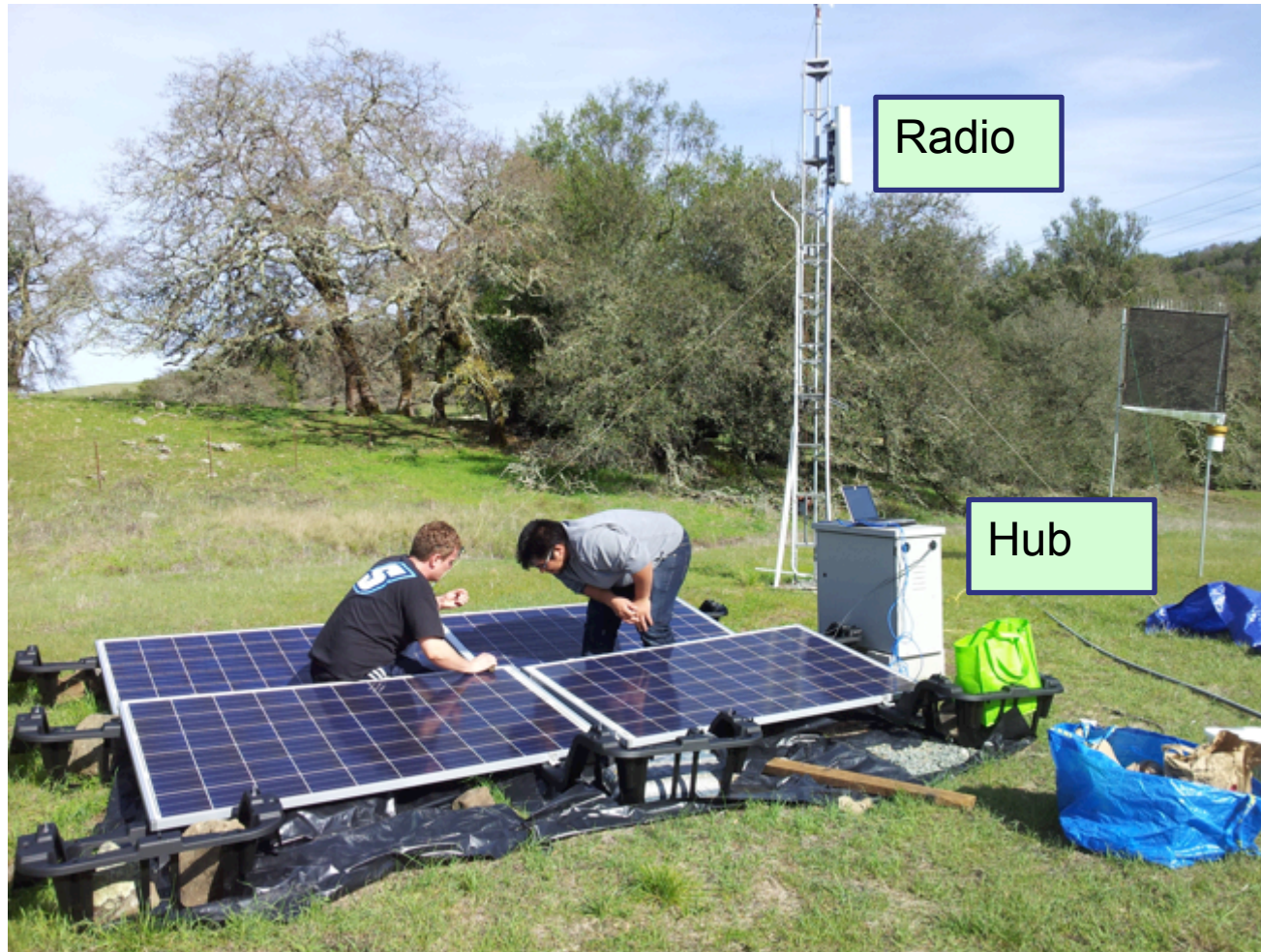
Prop. Constant $\gamma(f)|_{f=3.4 \text{ kHz}} = \sqrt{(180 + j6.8\pi \times 0.673)(0 + j6.8\pi \times 0.05 \times 10^{-3})}$
 $= 0.2979 + j0.3227 = 0.4392 \angle 47.3^\circ$

Transfer Function $H_{TWP}(f)|_{f=3.4 \text{ kHz}} = e^{-6 \times \gamma(f)|_{f=3.4 \times 10^3}} = e^{-(0.2979 + j0.3227) \times 6}$
 $= -0.0598 - j0.1563 = 0.1674 \angle -110.9^\circ$

Output Signal $y(t) = |H_{TWP}(f)|_{f=3.4 \text{ kHz}} \times 5 \cos[6800\pi t + \angle H_{TWP}(f)|_{f=3.4 \text{ kHz}}]$
 $= 5 \times 0.1674 \cos(6800\pi t - 110.9^\circ) = 0.837 \cos(6800\pi t - 110.9^\circ)$

Example 2:

If the maximum run length using Category (Cat) 5 TWP from the antenna to the hub is about 100 feet, what is the expected power level at the hub assuming the radio outputs 250 mW at 100 MHz?



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If the maximum run length using Category (Cat) 5 TWP from the antenna to the hub is about 100 feet, what is the expected power level at the hub assuming the radio outputs 250 mW at 100 MHz?

- The attenuation of a Cat 5 TWP is given by

$$\text{Insertion Loss} = 8.686 \times 3.83 \times 10^{-3} \times \sqrt{10^8} \text{ dB/mile} = 8.686 \times 38.3 = 332.67 \text{ dB/mile}$$

- Thus:

$$\ell = 100 \text{ foot drop of Cat 5 TWP cable} = 332.67 \times 100/5000 = 6.65 \text{ dB.}$$

- Power at the radio is 250mW \rightarrow 24 dBm
- Thus at the hub, the power will be $24 - 6.65 = 17.35$ dBm or

$$\text{dBm} = 10^{17.35/10} = 54 \text{ mW}$$

References

- M. Farooque Mesiya, Contemporary Communication Systems, 2012 – Chapter 2
- Leon W. Couch II, Digital and Analog Communication Systems, 8th edition, Pearson / Prentice, Chapter 1
- Electronic Communications System: Fundamentals Through Advanced, Fifth Edition by Wayne Tomasi – Chapter 2
(https://www.goodreads.com/book/show/209442.Electronic_Communications_System)